Course Outline

1. Microwave Components
2. RF Propagation
3. Link Budget
4. Reliability
5. Interference Analysis
Microwave Diagram
Radio Equipment
Radio Equipment

- “Waterfall” Curves

Theoretical Error Performance of Digital Modulation Schemes

- BPSK
- 4 PSK
- QPSK
- 8 PSK
- 4 QAM
- 16 QAM
- 64 QAM
- 256 QAM

C/N (RF Carrier-to-Noise Ratio) dB

Log BER Probability (e.g. -6 = 10^-6 BER)

Excludes FEC Improvement
Radio Equipment

• **Threshold**
  – Minimum receiver input level below which BER becomes excessive due to thermal noise
    • The 10^-6 BER threshold is called the *Static Threshold*
    • The 10^-3 BER threshold is called the *Dynamic or Outage Threshold*

• **Oversaturation Level**
  – Maximum receiver input level above which BER becomes excessive due to overdriving electronics into saturation (distortion)

• **Receiver can operate with low error rate between threshold and oversaturation → dynamic range**
### North American Digital Hierarchy

<table>
<thead>
<tr>
<th>Designation</th>
<th>Data Rate</th>
<th>DS0's (No of VC)</th>
</tr>
</thead>
<tbody>
<tr>
<td>DS1 (T1)</td>
<td>1.544 Mb/s</td>
<td>24</td>
</tr>
<tr>
<td>DS2 (T2)</td>
<td>6.312 Mb/s</td>
<td>96</td>
</tr>
<tr>
<td>DS3 (T3)</td>
<td>45 Mb/s</td>
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<tr>
<td>3xDS3</td>
<td>135 Mb/s</td>
<td>2016</td>
</tr>
<tr>
<td>DS5 (T5)</td>
<td>400 Mb/s</td>
<td>5760</td>
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### European Digital Hierarchy

<table>
<thead>
<tr>
<th>Designation</th>
<th>Data Rate</th>
<th>DS0's (No of VC)</th>
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<tbody>
<tr>
<td>E1</td>
<td>2.048 Mb/s</td>
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</tr>
<tr>
<td>E2</td>
<td>8.448 Mb/s</td>
<td>128</td>
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<tr>
<td>E3</td>
<td>34.4 Mb/s</td>
<td>512</td>
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<tr>
<td>E4</td>
<td>139.3 Mb/s</td>
<td>2048</td>
</tr>
<tr>
<td>E5</td>
<td>565 Mb/s</td>
<td>8192</td>
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</table>

### Optical Signal Hierarchy

<table>
<thead>
<tr>
<th>SONET Designation</th>
<th>SDH Designation</th>
<th>Data Rate</th>
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<tbody>
<tr>
<td>STS-3</td>
<td>STM-1</td>
<td>155.52 Mb/s</td>
</tr>
<tr>
<td>STS-12</td>
<td>STM-4</td>
<td>622.08 Mb/s</td>
</tr>
<tr>
<td>STS-48</td>
<td>STM-16</td>
<td>2488.32 Mb/s</td>
</tr>
<tr>
<td>STS-192</td>
<td>STM-64</td>
<td>9953.28 Mb/s</td>
</tr>
</tbody>
</table>
Transmission Lines
Transmission Lines

• Maximum useful frequency is $f_{\text{max}}$, above which electromagnetic modes in addition to the fundamental mode can propagate introducing dispersion (distortion)

• Waveguides have a cutoff frequency $f_{\text{co}}$, the lowest frequency that will propagate along the waveguide without dying out

• Useful Frequency Ranges:
  - Coax: 0 to $f_{\text{max}}$
  - Waveguide: $f_{\text{co}}$ to $f_{\text{max}}$
Transmission Lines

<table>
<thead>
<tr>
<th>Transmission Line Loss (dB/100 ft)</th>
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<tbody>
<tr>
<td>Coaxial Cable</td>
</tr>
<tr>
<td>3/8” (SFX-500)</td>
</tr>
<tr>
<td>7/8” (FXL-780)</td>
</tr>
<tr>
<td>1-5/8” (FXL-1873)</td>
</tr>
<tr>
<td>Elliptical Waveguide</td>
</tr>
<tr>
<td>960 MHz</td>
</tr>
<tr>
<td>2.1 GHz</td>
</tr>
<tr>
<td>3.7 GHz</td>
</tr>
<tr>
<td>6.2 GHz</td>
</tr>
<tr>
<td>11 GHz</td>
</tr>
<tr>
<td>18 GHz</td>
</tr>
<tr>
<td>23 GHz</td>
</tr>
</tbody>
</table>
Direct Radiating Antennas focus the radio beam generally by using a feed source to illuminate a curved (Parabolic) reflecting surface.
Microwave Antennas

**Parabolic Reflector Antenna:** a feed illuminates a parabolic reflector to focus the radio beam in the desired direction

- Grid (ULine)
- Standard (PL, PAR)
- Ultra High Performance (UHP, UHX)
- ValuLine High Performance Low Profile (VHLP)
- Super High Performance (Sentinel SHP)
Microwave Antennas

- **Antenna Gain (Maximum Power Gain)**

\[ G = (\text{efficiency}) \times \left( \frac{\text{maximum radiation intensity}}{\text{isotropic radiation intensity}} \right) \]

- Gain is inversely proportional to beamwidth
- Gain is directly proportional to reflector size, operating frequency and efficiency
Antenna Gain

\[
G = 10 \log \left( \frac{4\pi e A}{\lambda^2} \right) dB_i
\]

\[
= 10 \log e \left( \frac{\pi df}{c} \right)^2 dB_i
\]

G = Antenna Gain in dBi (reference to isotropic radiator)
e = Antenna efficiency: 0.5 < e < 0.7, typically 0.55
A = Area of aperture (reflective surface) in units of wavelength
\( \lambda \) = Wavelength = \( c/f \)
c = Speed of light \( \approx 3.0 \times 10^8 \) m/s
f = Frequency (Hz)
d = Antenna diameter
Microwave Antennas

• Not possible to construct perfect antennas
  – Highest gain concentrated in region near main beam, but lower gains exist in other directions
  – The off-axis response presents a potential for interference from or into the antenna

• Discrimination
  – Ratio (expressed in dB) of the gain at an off-axis angle to the main beam (maximum on-axis) gain
  – Influenced by
    • Quality / Performance Level of antenna
    • Direction (Discrimination Angle)
    • Polarization (Vertical or Horizontal)
Microwave Antennas

- **Beamwidth**
  - Angle between the half-power (3 dB) points of the main beam
  - Figure-of-merit on how effectively the antenna concentrates the radiated power in the desired direction

3 dB Beamwidth 1.8°
Microwave Antennas

• For a Given Antenna Size, Directionality Depends on:
  - Frequency
  - Performance Category

<table>
<thead>
<tr>
<th>Parabolic Diameter (ft)</th>
<th>Performance</th>
<th>Band (GHz)</th>
<th>Gain (dBi)</th>
<th>Beamwidth (deg)</th>
<th>F/B Ratio (dB)</th>
</tr>
</thead>
<tbody>
<tr>
<td>6</td>
<td>Standard</td>
<td>6.2</td>
<td>38.9</td>
<td>1.8</td>
<td>46.0</td>
</tr>
<tr>
<td>6</td>
<td>Ultra High</td>
<td>6.2</td>
<td>38.8</td>
<td>1.8</td>
<td>75.0</td>
</tr>
<tr>
<td>6</td>
<td>Standard</td>
<td>11</td>
<td>44.0</td>
<td>1.0</td>
<td>51.0</td>
</tr>
<tr>
<td>6</td>
<td>Ultra High</td>
<td>11</td>
<td>44.0</td>
<td>1.1</td>
<td>80.0</td>
</tr>
</tbody>
</table>
Microwave Antennas

Radiation Pattern Envelope

Antenna Type Number: UHP10-59W
10.0 Foot Antenna: 5.925 - 7.125 GHz Single Polarized
Gain: 43.29 ± 0.2 dBi at 6.425 GHz

- Envelope for a Horizontally Polarized Antenna (HH,HV)
- Envelope for a Vertically Polarized Antenna (VW,WH)

Feed is installed as illustrated with the red painted half of the hub positioned toward the 270° azimuth LEFT side of the antenna.

ANDREW CORPORATION

For further information, ask for Andrew Bulletin 1032, "Radiation Pattern Envelopes."

ANDREW CORPORATION

This antenna meets FCC Part 21 Performance Requirements.
This antenna meets FCC Part 94 Performance Requirements.
Antenna ID Code: 53500A

Additionally, the graph shows the azimuth directivity comparison with expanded scales.
Microwave Antennas

• **Antenna Field Patterns**
  - Near field: Radiation Pattern not well formed
  - Transition: Pattern begins to form but still depends on distance
    - Near/Transition Boundary $\pi D^2/(8\lambda)$
  - Far field: Pattern fully formed and independent of distance
    - Transition/Far Boundary at $2D^2/\lambda$
RF Propagation
RF Propagation

• **Some Basics**
  - Frequency \((f)\) — Number of repetitions (cycles) per second (Hz)
  - Period \((\tau)\) — Duration of a Single Cycle (seconds)
  - Wavelength \((\lambda)\) — Distance wave travels in one period
  - Speed of Light \((c)\) = \(2.99792458 \times 10^8\) m/s

\[
f = \frac{1}{\tau} = \frac{c}{\lambda}
\]
Free Space Path Loss

• The difference between power transmitted & power received is called *Path Loss*

• The portion of Path Loss attributed to the spreading effect of signal is referred to as Free Space Path Loss

• Free Space Path Loss is inversely proportional to the square of the wavelength
Free Space Path Loss

- The Free Space Path Loss Equation(s):
  - \( FSPL_{\text{mi}} = 96.6 + 20\log(f_{\text{GHz}}) + 20\log(d_{\text{mi}}) \) dB
  - \( FSPL_{\text{km}} = 92.4 + 20\log(f_{\text{GHz}}) + 20\log(d_{\text{km}}) \) dB

- Example:
  - What’s the FSPL for a 20 mi path at 6.175 GHz?
  - \( FSPL = 96.6 + 20\log(6.175) + 20\log(20) \) dB = 138.4 dB
  - What’s the FSPL at 10 mi? 40 mi?
Atmospheric Absorption

**Figure 5**
Specific attenuation due to atmospheric gases

- Frequency, $f$ (GHz)
- Specific attenuation (dB/km)

- Pressure: 1013 hPa
- Temperature: 15°C
- Water vapor: 7.5 g/m³
Fresnel Zone

\[ r = 17.3 \sqrt{\frac{(d_1 + d_2)}{F \cdot (d_1 + d_2)}} \]

- \(d\) = Distance between antenna
- \(d_1\) = Distance to point-of-interest from antenna 1
- \(d_2\) = Distance to point-of-interest from antenna 2
- \(r\) = Radius of Fresnel Zone at point-of-interest
- \(F\) = Frequency in GHz
Fresnel Zones

- Reflections from objects at the surface of *odd* numbered Fresnel zones will add *in phase* at the receiver
  - \((180^\circ \text{ shift } + n \times \frac{1}{2} \text{ wavelengths})\)
Fresnel Zones

- Reflections from objects at the surface of even numbered Fresnel zones will be *anti-phase* at the receiver
  - $(180^\circ \text{ shift} + n \text{ wavelengths})$
Fresnel Zone Diagram

Where:

\[ F_n = 72.1 \sqrt{\frac{nd_1d_2}{fD}} \]

- \( F_n \) = \( n \)th Fresnel Zone radius in feet
- \( d_1 \) = distance from one end of the path to the reflection point in miles
- \( D \) = total path length
- \( d_2 = D - d_1 \)
- \( f \) = frequency in GHz
Fresnel Zone Examples

\[ F_n = 72.1 \sqrt{\frac{nd_1d_2}{fD}} \]

If:

- D = 30 mi
- D = 30 mi
- D = 8 mi
- D = 3 mi
- d_1 = d_2 = 15 mi
- d_1 = d_2 = 15 mi
- d_1 = d_2 = 4 mi
- d_1 = d_2 = 1.5 mi
- f = 1.9 GHz
- f = 6.7 GHz
- f = 23 GHz
- f = 38 GHz

Then:

- F_1 = 143.25 ft
- F_1 = 76.3 ft
- F_1 = 21.3 ft
- F_1 = 10.3 ft
Path clearance less than 0.6*F₁ can result in additional path loss due to diffraction.
K Factor
• This causes a bending of the rays from the transmitter to the receiver
  – The ray bends up for typically negative $dn/dh$
However, if $dn/dh$ is positive, the ray bends down towards the ground.
K Factor

- Worldwide map of dN/dh (ΔN)

FIGURE B-15. Annual mean of refractivity gradient between surface and 1 km, ΔN.
K Factor

- It is convenient to model the bending ray as an increase in the curvature of the earth, leaving the ray straight
Now, we have a relationship between the effective earth radius, $a_e$ and the actual earth radius $a$ (6370 km):

\[
a_e = ka
\]

or

\[
k = a / a_e
\]

\[
= 1/(1+a(dn/dh))
\]

\[
= 1/(1+a(dN/dh) \times 10^{-6})
\]

plugging for $a$:

\[
k = 157 / (157 + dN/dh)
\]
K Factor

- Earth bulge (h):

\[ h = \frac{d_1 d_2}{12.75k} \text{ meters} \]

\[ h = 0 \text{ for } k = \text{infinity} \]
Path Clearance
Path Clearance

- Path profile
Path Clearance

- Proper Path Clearance
Path Clearance

• Excessive Path Clearance
Reliability
Reliability

Outage

• Time that the RSL is faded below the Receiver Threshold is *outage*

• Outage is calculated as time below $10^{-6}$ BER for most purposes

• In the past, outage was calculated as time below $10^{-3}$ BER for telephony since the PCM multiplexers lose framing just below this BER
Reliability

**Fade Margin**

- The amount the signal may fade before a path outage results
- Digital—Composite Fade Margin
  - Includes a Thermal (or Flat) Fade Margin term that is the difference between the normal RSL and the minimum usable signal (Receiver Threshold) level. Also includes terms taking into account the effect of frequency selective fading in the channel (Dispersive Fade Margin) and the effect of interference (External Interference Fade Margin)
Reliability

• Composite Fade Margin Equation

\[ CFM = -10 \log \left( 10^{-\frac{DFM}{10}} + 10^{-\frac{TFM}{10}} + 10^{-\frac{EIFM}{10}} + 10^{-\frac{AIFM}{10}} \right) \]

CFM = Composite fade margin
DFM = Dispersive fade margin
TFM = Thermal fade margin \((Receive \ level - Threshold)\)
EIFM = External interference fade margin
AIFM = Adjacent-channel interference fade margin
Reliability

• Example:

If the RSL is -40 dBm, the Receiver Threshold is -75 dBm, the Dispersive Fade Margin is 50 dB, and the External Interference Fade Margin is 60 dB, what is the Composite Fade Margin of the link?

- TFM = -40 - (-75) = 35
- CFM = -10\log_{10}(10^{-5}+10^{-3.5}+10^{-6})
  
  34.85 dB
• The fade margin must be high enough to allow the path to meet the reliability objective

• Vigants (1975) gave a formula for predicting the link outage time based on the fade margin

• Outage time is dependent on:
  – climate, terrain, temperature, frequency, and path length

• Outage time can be greatly reduced by using frequency and/or space diversity
Reliability

- There are 31,536,000 seconds in a year

- An availability of 99.99% (four nines) means an outage of 3153.5 seconds per year, or about 53 minutes

- An availability of 99.999% (five nines) means an outage of 315.35 seconds per year, or about 5 minutes
Reliability

- **Vigants Multipath Outage Model**
  - Predicts *Atmospheric* Multipath Fading

\[
T = \frac{rT_0 \times 10^{-\left(\frac{CFM}{10}\right)}}{I_0}
\]

Where:
- \( T \) = annual outage time (s)
- \( r \) = fade occurrence factor
- \( T_0 = \frac{t}{50}(8\times10^6) \) = length of the fading season (s)
- \( t \) = average annual temperature (F)
- \( CFM \) = Composite Fade Margin (dB)
- \( I_0 \) = SD Improvement Factor (1 for non-diversity, >1 for diversity)
Reliability

- Space Diversity Improvement Factor

\[ I_0 = 7 \times 10^{-5} s^2 \left( \frac{f}{D} \right) 10^{\left( \frac{CFM}{10} \right)} \]

Where:

- \( s \) = vertical antenna spacing (ft) (\( s \leq 50 \) feet)
- \( f \) = frequency (GHz)
- \( D \) = path length (mi)
- \( CFM \) = composite fade margin (dB)
• **Space Diversity Improvement Factor**

  - Example: Our 30 mile 6 GHz link has a Composite Fade Margin of 35 dB. If we add space diversity antennas 20 feet below the main antennas, by what factor do we predict that the atmospheric multipath fading outage will be reduced?

  \[ Io = (7 \times 10^{-5})(20^2)(6/30)(10^{3.5}) = 17.7 \]
Reliability

• Fade Occurrence Factor

$$r = x\left(\frac{50}{w}\right)^{1.3} \left(\frac{f}{4}\right)D^3 \times 10^{-5}$$

Where:

- \(x\) = Climate factor (0.5 - 2 for poor - good areas, see map)
- \(w\) = Terrain roughness (20 ≤ \(w\) ≤ 140 ft.)
- \(f\) = frequency (GHz)
- \(d\) = Path length (mi)
Reliability

- Climate Factor

Hawaii / Caribbean: \( x = 2 \)  
Alaska:  
  - \( X = 0.5 \) for coastal & mountainous areas  
  - \( X = 1 \) for flat, permafrost tundra areas
Reliability

- **Fade Occurrence Factor Example**
  
  - For an area of average propagation \((x = 1)\) and a 30 mile path of average terrain roughness \((w=50')\), what is the fade occurrence factor at 6 Ghz?
  
  - \(r = (1)(50/50)^{1.3}(6/4)(30^3)(10^{-5}) = 0.405\)
Reliability

• Outage Example

  - Our link has a CFM of 35 dB and a fade occurrence factor of 0.405. If the average annual temperature is 60° F, what is the expected annual outage due to atmospheric multipath fading without diversity?

  - $T_0 = (60/50)(8\times10^6) = 9.6\times10^6$ s
  - $T = (0.405)(9.6\times10^6)(10^{-3.5}) = 1230$ s
• **Space Diversity Improvement Example**
  
  – The annual outage of 1230 s expected on this link doesn't meet the standard that we have established for our network. We calculate a space diversity improvement factor of 17.7 for a 20' antenna spacing. What annual outage do we expect with space diversity?
  
  – \( T = \frac{1230}{17.7} = 70 \text{ s} \)
Reliability

• Rain Outage
  – Rain fades become significant when the frequency is above 10 GHz
  – Crane model predicts fade depth probability based on rainfall rate statistics by region (map)
  – Outage probability proportional to rain rate—*not* total annual rainfall
Reliability

• Rain Rate Climate Regions (Crane)
Interference Calculations
Interference Calculations

- **C/I**: The ratio of desired signal power to interference power at the receiver input

\[ C/I = C(dBm) - I(dBm) \]
Interference Calculations

- **Interference Level at B**

\[
I_B = P_D + G_D - L_D - FSPL_{DB} + G_B - L_B - D_{Total}
\]

- \( P_D \): Transmit Power at D
- \( G_D \): Antenna Gain at D
- \( L_D \): Fixed Losses at D
- \( FSPL_{DB} \): Free Space Path Loss from D to B
- \( G_B \): Antenna Gain at B
- \( L_B \): Fixed Losses at B
Interference Calculations

• Total Discrimination

<table>
<thead>
<tr>
<th>Antenna D @ α</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>VV</td>
<td>5</td>
</tr>
<tr>
<td>VH</td>
<td>34</td>
</tr>
<tr>
<td>HH</td>
<td>6</td>
</tr>
<tr>
<td>HV</td>
<td>35</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Antenna B @ β</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>VV</td>
<td>13</td>
</tr>
<tr>
<td>VH</td>
<td>29</td>
</tr>
<tr>
<td>HH</td>
<td>9</td>
</tr>
<tr>
<td>HV</td>
<td>32</td>
</tr>
</tbody>
</table>
Interference Calculations

• Example

We suspect that a transmitter 40 miles away is a source of potential interference to a receiver on our 20 mile 6.175 GHz path. The power of both transmitters is 1 W (30 dBm). Assuming that all antenna gains are 40 dB, all line losses are 0 dB, that we are concerned about VV interference, and that the total discrimination is 18 dB as calculated on the previous slide, what is the C/I?

\[
\begin{align*}
C &= 30 + 40 - 138.4 + 40 = -28.4 \text{ dBm} \\
I &= 30 + 40 - 144.4 + 40 - 18 = -52.4 \text{ dBm} \\
C/I &= -28.4 - (-52.4) = 24 \text{ dB}
\end{align*}
\]
Frequency Planning

• Earth Station Interference
Thank You

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